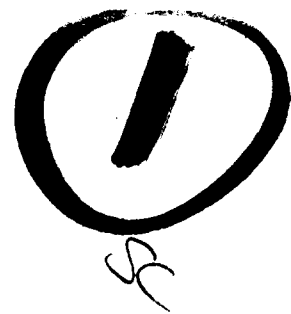


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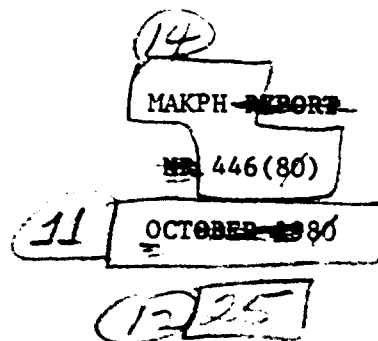
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HEADQUARTERS  
OGDEN AIR LOGISTICS CENTER  
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(6)  
QUALIFICATION OF A NEW MAPO  
SOURCE AND ERL-510 CURING AGENT  
FOR MINUTEMAN STAGE 1 UF-2121 LINER.

*John A. Thompson*  
(20)

PROPELLANT ANALYSIS LABORATORY



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QUALIFICATION OF A NEW MAPO  
SOURCE AND ERL-510 CURING AGENT  
FOR MINUTEMAN STAGE 1 UF-2121 LINER

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ABSTRACT

Thiokol Chemical Corporation/Wasatch Division uses MAPO in the production of UF-2121 liner. Thiokol changed MAPO vendors and, therefore, qualification of the new source MAPO was required.

Thiokol prepared specimens from the new source and also specimens from the original source which are to be used as the control material in the 10 year surveillance testing program. The specimens were transferred to Ogden ALC for testing and reporting of the data obtained.

This report includes the test results for the first, second, third, fourth, fifth, and sixth time testing of the control and special specimens at Ogden ALC.

Statistical analysis of the test data showed that the physical properties of the new source compared closely to the old source of UF-2121 liner specimens.

In all instances, the mean data for the control and special specimens are well above the minimum requirements found in TWR-7857 REV A, Thiokol specimen data. Therefore, the capability of the liner from the new source material is expected to perform satisfactorily.

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## INTRODUCTION

### A. PURPOSE:

Quality assurance testing of specimens prepared from the new source of MAPO to assure that liner material for First Stage Minuteman Motors will perform as predicted.

### B. BACKGROUND:

\*Tris [1-(2 methyl) aziridinyl] phosphine oxide (MAPO) is used as a curing agent in the Minuteman Stage One UF-2121 liner. MAPO was produced by Immont Chemical (Immont) and shipped to Arsynco Incorporated (Arsynco) for purification and marketing. Immont sold the production rights for MAPO to Arsynco and terminated the production of raw MAPO in 1972.

Since MAPO is a critical ingredient in UF-2121 liner formulation, the source change for the manufacture of MAPO was considered a serious change. Therefore, it was necessary for Thiokol to conduct qualification testing on liner material using MAPO manufactured by Arsynco before it could be considered acceptable for use in Minuteman Stage I UF-2121 liner.

ERLA-500 was the qualified epoxy curing agent used with MAPO in the UF2121 liner. Union Carbide terminated their process for ERLA-500. ERLA-510 used in similar liners (i.e. UF-2137) was substituted for ERLA-500 and qualified with MAPO from the new source.

The test conditions and test methods are shown in Table I.

\*TWR-7857 Rev A Report, J. W. Rabern

Qualification testing was performed by Thiokol and reported in TWR-7857 Rev A. In addition, specimens were prepared by Thiokol from the new vendor's material and from the old source material for a "follow on" test program. These specimens were then transferred to Ogden ALC for a continuing surveillance test program designed to cover a ten year span. The material from the old source will be used as the control samples.

The ten year sampling plan is shown below. Those specimens identified for the sixth year were tested at this test period. The types of specimens are Disc (steel/liner/steel), Cup (steel/liner/TP-H1011), and Peel (broadcloth/liner/TP-H1011). For the disc specimen, the adhesion between the liner and steel is the critical factor. For the cup specimen, the adhesion between the propellant and the liner is critical. For the peel specimen the propellant to liner peel strength when pulled at 180° is critical.

#### TEN YEAR CONTINGENCY AGING SAMPLE CODING

| Age<br>(yr) | Storage<br>Temp<br>(°F) | Disc (Sample Nr) |           | Cup (Sample Nr) |           | Peel (Sample Nr) |           |
|-------------|-------------------------|------------------|-----------|-----------------|-----------|------------------|-----------|
|             |                         | Control*         | Special** | Control*        | Special** | Control*         | Special** |
| 1           | 75                      | 1 - 6            | 181-186   | 61-66           | 241-246   | 121-126          | 301-306   |
| 2           | 75                      | 7 -12            | 187-192   | 67-72           | 247-252   | 127-132          | 307-312   |
| 3           | 75                      | 13-18            | 193-198   | 73-78           | 253-258   | 133-138          | 313-318   |
| 4           | 75                      | 19-24            | 199-204   | 79-84           | 259-264   | 239-144          | 319-324   |
| 5           | 75                      | 25-30            | 205-210   | 85-90           | 265-270   | 145-150          | 325-330   |
| 6           | 75                      | 31-36            | 211-216   | 91-96           | 271-276   | 151-156          | 331-336   |
| 7           | 75                      | 37-42            | 217-222   | 97-102          | 277-282   | 157-162          | 337-342   |
| 8           | 75                      | 43-48            | 223-228   | 103-108         | 283-288   | 163-168          | 343-348   |
| 9           | 75                      | 49-54            | 229-234   | 109-114         | 289-294   | 169-174          | 349-354   |
| 10          | 75                      | 55-60            | 235-240   | 115-120         | 295-300   | 175-180          | 355-360   |

\* Liner mix A73-11846 - control or old MAPO source material

\*\* Liner mix A73-11810 - Experimental MAPO

TABLE I

## Test Conditions and Methods

| <u>Group</u>               | <u>Test</u>                     | <u>Condition</u>   | <u>Config-<br/>uration</u> | <u>G085<br/>Spec<br/>Code</u> | <u>Spec<br/>Per<br/>Cond</u> | <u>Total<br/>Number<br/>of Spec</u> | <u>Test<br/>Method</u> |
|----------------------------|---------------------------------|--|----------------------------|-------------------------------|------------------------------|-------------------------------------|------------------------|
| Bond in<br>Tension<br>Disc | Tensile<br>Adhesion<br>OI#127-3 | CHS 0.5 in/<br>min, Chart 5.0<br>in/min, 500<br>lbs full scale<br>load 77°F ± 2° | Discs                      | TV                            | Control<br>6<br>Special<br>6 | 12                                  | A                      |
| Bond in<br>Tension<br>Cup  | Tensile<br>Adhesion<br>OI#127-3 | CHS 0.5 in/<br>min, Chart 5.0<br>in/min, 200 lbs<br>full scale load<br>77°F ± 2° | Cup                        | TC                            | Control<br>6<br>Special<br>6 | 12                                  | A                      |
| 180°<br>Peel<br>Specimens  | Tensile<br>Peel<br>OI#127-3     | CHS 10 in/min<br>77°F ± 2°<br>Chart 5 in/<br>min 20 lbs<br>full scale load       | Peel                       | TE                            | Control<br>6<br>Special<br>6 | 12                                  | B                      |

## TEST CONDITIONS

A. Testing of tensile adhesion specimens was performed using an Instron testing instrument. Properties measured were maximum stress to the nearest pound and failure mode.

Steel disc specimens require a stress of about 240 psi. The recommended initial full scale load is 500 pounds. This instrument setting should be changed to another setting if the first reading goes off scale on the high side. If 500 psi is exceeded, then change the reading to 1000 psi full scale.

Cup adhesion specimens are tested with a stress of 200 lbs per sq inch; the recommended full scale load is 500 lbs.

B. Testing of 180° peel samples was performed using an Instron testing instrument. The physical property of the material to be determined was the average peel strength to the nearest pound per inch.

NOTE: Thiokol's procedure for Testing and Laboratory Mixing of UF-2121 Liner. SLP 400, 28 April 71.

## STATISTICAL ANALYSIS

UF-2121 liner material is being tested under a ten year program to determine whether or not differences exist between liner materials manufactured from two separate sources of curing agent (MAPO). Test specimens were manufactured in two groups; control, using original source curing agent, and special, using new source curing agent. The test specimens for these two groups are of three kinds; disc, cup, and peel. For each specimen type within each test group the sample test size is six. Laboratory testing for six test periods or six years has been accomplished. Test data for the years 1975, 1976, 1977, 1978, 1979, and 1980 are in Tables 2 through 7, and columns are summarized using means and standard deviations.

With six test periods accomplished, regression plots (Figures 1 - 6) were made to determine whether slope and elevation differences existed between control and special test data. No differences in either slope or elevation were found. The regression model  $Y = a + bx$ , using individual data points, was used in the regression analyses. The variance about the least squares trend line is used to compute a tolerance interval such that at the 90% confidence level 90% of the sample distribution falls within this interval. This tolerance interval is extrapolated 24 months past the age point pertaining to the oldest specimens tested. The statistical significance of the slope of the trend line is evaluated for each regression plot. If significant, it is an indication that change over time is occurring.

In determining differences in data pertaining to the two MAPO sources, analysis of covariance was employed to compare control and special data from



the regressions for each of the three types of test specimens. For analysis of covariance results, see Table 8. Taken at the five percent significance level, the only difference found was in disc data in the variance of the data away from the regression line.

## TEST RESULTS

The 1980 test data and the mean for the respective control and special data are shown in Table 7. In addition, for a convenient comparison, the 1975 through 1979 test data are included in Tables 2 through 6.

The statistical analysis results for the 1980 testing are shown in Table 8 with the regressions shown in Figures 1 through 6.

### DISC:

A statistically significant difference is shown for variance of test data in the MAPO source (Table 6) with no significant difference for the slope and elevation of the regression curves (Table 8).

The regression curves show a statistically significant gradual decrease for both the control and special sample data (Figures 1 & 2).

For the year 1980, the mean of the control and special data is 15.06 and 14.28 kg/sq cm respectively.

The minimum specification requirement according to TWR-7857 REV A, is 12.30 kg/sq cm minimum. As seen in Table 7, MAKPH's data is well above this minimum.

The failure mode was 100% cohesive in the liner for both the control and special specimens.

### CUP:

There is no significant difference in variance, slope or elevation when comparing control and special regression data (Table 8).

The regression curves show a statistically significant gradual decrease in maximum stress as the specimens age (Figures 3 & 4).

According to TWR-7857 REV A report, the minimum requirement is 4.92 kg/sq cm. The data means are 10.00 kg/sq cm for the control and 10.49 kg/sq cm for the special specimens.

The failure mode for the control and special specimens was 100% adhesive liner to propellant.

PEEL:

No significant difference is shown for the variance, slope or elevation when comparing control with special regression data (Table 8).

The regression curves (Figures 5 & 6) show a statistically significant gradual increase in peel strength with respect to the age of the specimens.

Thiokol reported (TWR-7857 REV A) 0.679 and 0.732 \*kg/L cm respectively for the control and special mean data at age six months. This compares with 1980 data of 1.09 and 1.08 kg/l cm respectively for control and special mean data (Table 7).

The mode of failure was 100% liner to propellant bond.

\* Kilograms per linear centimeter

## CONCLUSIONS

Based on this analysis, the only statistically significant difference between the control and special specimens is the variance for disc specimens.

The regressions show a gradual statistically significant change.

The strength of specimens is well above the required minimum for disc and cup, and above that reported in Thiomol testing for peel.

From the data analysis, the new source of raw material performs as well as the old source; and therefore is expected to perform satisfactorily.

## RECOMMENDATIONS

It is recommended that the testing plan be continued to assure long range capability of the liner produced from the new source of material.

TABLE 2  
TEST DATA SUMMARY  
JULY 1975

| DISC      |                    |         |                    | CUP     |                    |         |                    | PEEL    |         |         |         |
|-----------|--------------------|---------|--------------------|---------|--------------------|---------|--------------------|---------|---------|---------|---------|
| Control   |                    | Special |                    | Control |                    | Special |                    | Control |         | Special |         |
| Nr        | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/L-Cm | Nr      | Kg/L-Cm |
| 1         | 17.085             | 181     | 17.225             | 61      |                    | 241     | 11.601             | 121     | 0.6786  | 301     | 0.6786  |
| 2         | 17.507             | 182     | 17.858             | 62      | 11.812             | 242     | 11.601             | 122     | 0.6786  | 302     | 0.6965  |
| 3         | 17.225             | 183     | 17.015             | 63      | 11.741             | 243     | 11.531             | 123     | 0.7143  | 303     | 0.6965  |
| 4         | 17.929             | 184     | 16.944             | 64      | 12.163             | 244     | 11.671             | 124     | 0.7500  | 304     | 0.6965  |
| 5         | 17.366             | 185     | 17.436             | 65      | 12.234             | 245     | 11.390             | 125     | 0.7679  | 305     | 0.7143  |
| 6         | 17.296             | 186     | 19.054             | 66      | 11.882             | 246     | 11.390             | 126     | 0.7858  | 306     | 0.6965  |
| $\bar{Y}$ | 17.401             |         | 17.589             |         | 11.966             |         | 11.531             |         | 0.7292  |         | 0.6965  |
| S         | 0.2943             |         | 0.7899             |         | 0.2191             |         | 0.1176             |         | 0.0458  |         | 0.0113  |

TABLE 3  
TEST DATA SUMMARY  
MAY 1976

| DISC      |                    |         |                    | CUP     |                    |         |                    | PEEL    |         |         |         |
|-----------|--------------------|---------|--------------------|---------|--------------------|---------|--------------------|---------|---------|---------|---------|
| Control   |                    | Special |                    | Control |                    | Special |                    | Control |         | Special |         |
| Nr        | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/L-Cm | Nr      | Kg/L-Cm |
| 7         | 15.116             | 187     | 14.483             | 67      |                    | 247     | 13.288             | 127     | 0.9643  | 307     | 1.0536  |
| 8         | 16.311             | 188     | 14.905             | 68      | 13.710             | 248     | 13.710             | 128     | 0.9286  | 308     | 1.0358  |
| 9         | 15.397             | 189     | 14.483             | 69      | 13.640             | 249     | 13.640             | 129     | 0.9286  | 309     | 1.0179  |
| 10        | 15.960             | 190     | 14.765             | 70      | 13.007             | 250     | 13.077             | 130     | 1.0179  | 310     | 1.0358  |
| 11        | 15.819             | 191     | 15.468             | 71      | 13.148             | 251     | 13.359             | 131     | 1.1072  | 311     | 1.0536  |
| 12        | 14.554             | 192     | 14.765             | 72      | 13.499             | 252     | 13.499             | 132     | 1.0001  | 312     | 1.0358  |
| $\bar{Y}$ | 15.526             |         | 14.812             |         | 13.401             |         | 13.429             |         | 0.9911  |         | 1.0388  |
| S         | 0.6356             |         | 0.3633             |         | 0.3088             |         | 0.2354             |         | 0.0675  |         | 0.0134  |

NOTE: Kg/L-Cm = Kilograms per linear centimeter. Also, for the peel test the results are in average peel.

TABLE 4  
TEST DATA SUMMARY  
APRIL 1977

| DISC      |                    |         |                    | CUP     |                    |         |                    | PEEL    |         |         |         |
|-----------|--------------------|---------|--------------------|---------|--------------------|---------|--------------------|---------|---------|---------|---------|
| Control   |                    | Special |                    | Control |                    | Special |                    | Control |         | Special |         |
| Nr        | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/L-Cm | Nr      | Kg/L-Cm |
| 13        | 17.155             | 193     | 17.436             | 73      | 9.281              | 253     | 9.140              | 133     | 0.7322  | 313     | 0.7358  |
| 14        | 16.522             | 194     | 16.874             | 74      | 9.281              | 254     | 9.070              | 134     | 0.7143  | 314     | 0.7358  |
| 15        | 16.874             | 195     | 16.944             | 75      | 8.999              | 255     | 8.999              | 135     | 0.6736  | 315     | 0.7358  |
| 16        | 17.015             | 196     | 17.366             | 76      | 9.281              | 256     | 9.140              | 136     | 0.7500  | 316     | 0.7143  |
| 17        | 16.874             | 197     | 17.015             | 77      | 9.492              | 257     | 8.367              | 137     | 0.7500  | 317     | 0.7500  |
| 18        | 16.874             | 198     | 17.015             | 78      | 9.281              | 258     | 8.789              | 138     | 0.6429  | 318     | 0.7143  |
| $\bar{X}$ | 16.886             |         | 17.108             |         | 9.269              |         | 8.918              |         | 0.7113  |         | 0.7560  |
| S         | 0.2107             |         | 0.2337             |         | 0.1570             |         | 0.2994             |         | 0.0429  |         | 0.0352  |

TABLE 5  
TEST DATA SUMMARY  
JUNE 1978

| DISC      |                    |         |                    | CUP     |                    |         |                    | PEEL    |         |         |         |
|-----------|--------------------|---------|--------------------|---------|--------------------|---------|--------------------|---------|---------|---------|---------|
| Control   |                    | Special |                    | Control |                    | Special |                    | Control |         | Special |         |
| Nr        | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/Cm <sup>2</sup> | Nr      | Kg/L-Cm | Nr      | Kg/L-Cm |
| 19        | 14.906             | 199     | 14.554             | 79      | 10.898             | 259     | 10.406             | 139     | 0.9109  | 319     | 1.0180  |
| 20        | 14.624             | 200     | 14.695             | 80      | 10.968             | 260     | 10.476             | 140     | 0.9823  | 320     | 1.0359  |
| 21        | 14.695             | 201     | 14.343             | 81      | 10.617             | 261     | 10.616             | 141     | 0.9466  | 321     | 1.0180  |
| 22        | 14.906             | 202     | 14.343             | 82      | 10.125             | 262     | 10.125             | 142     | 1.0002  | 322     | 1.0359  |
| 23        | 14.343             | 203     | 14.624             | 83      | 10.406             | 263     | 10.687             | 143     | 1.0716  | 324     | 1.0537  |
| 24        | 15.187             | 204     | 14.414             | 84      | 10.476             | 264     | 10.125             | 144     | 0.9466  | 326     | 0.9287  |
| $\bar{X}$ | 14.777             |         | 14.496             |         | 10.582             |         | 10.406             |         | 0.9764  |         | 1.0150  |
| S         | 0.2898             |         | 0.1503             |         | 0.3166             |         | 0.2391             |         | 0.0561  |         | 0.0444  |

TABLE 6

TEST DATA SUMMARY  
11 JUNE 1979

| DISC      |                    |         |                    | CUP     |                    |         |                    | PEEL    |         |         |         |
|-----------|--------------------|---------|--------------------|---------|--------------------|---------|--------------------|---------|---------|---------|---------|
| Control   |                    | Special |                    | Control |                    | Special |                    | Control |         | Special |         |
| Nr        | kg/cm <sup>2</sup> | Nr      | kg/cm <sup>2</sup> | Nr      | kg/cm <sup>2</sup> | Nr      | kg/cm <sup>2</sup> | Nr      | kg/L-cm | Nr      | kg/L-cm |
| 25        | 17.015             | 205     | 17.436             | 85      | 9.632              | 265     | 9.562              | 145     | 0.8572  | 325     | 0.7679  |
| 26        | 16.874             | 206     | 16.874             | 86      | 9.703              | 266     | 9.140              | 146     | 0.8393  | 326     | 0.7679  |
| 27        | 16.874             | 207     | 16.593             | 87      | 9.773              | 267     | 9.562              | 147     | 0.8572  | 327     | 0.9643  |
| 28        | 16.944             | 208     | 16.522             | 88      | 9.632              | 268     | 9.281              | 148     | 0.8572  | 328     | 0.7143  |
| 29        | 16.804             | 209     | 16.382             | 89      | 9.632              | 269     | 9.421              | 149     | 0.7679  | 329     | 0.7143  |
| 30        | 16.171             | 210     | 17.366             | 90      | 9.492              | 270     | 9.421              | 150     | 0.8036  | 330     | 0.7500  |
| $\bar{Y}$ | 16.780             |         | 16.862             |         | 9.644              |         | 9.398              |         | 0.8304  |         | 0.7798  |
| S         | 0.3070             |         | 0.4477             |         | 0.0934             |         | 0.1644             |         | 0.0370  |         | 0.0936  |

TABLE 7

TEST DATA SUMMARY  
SEPTEMBER 1980

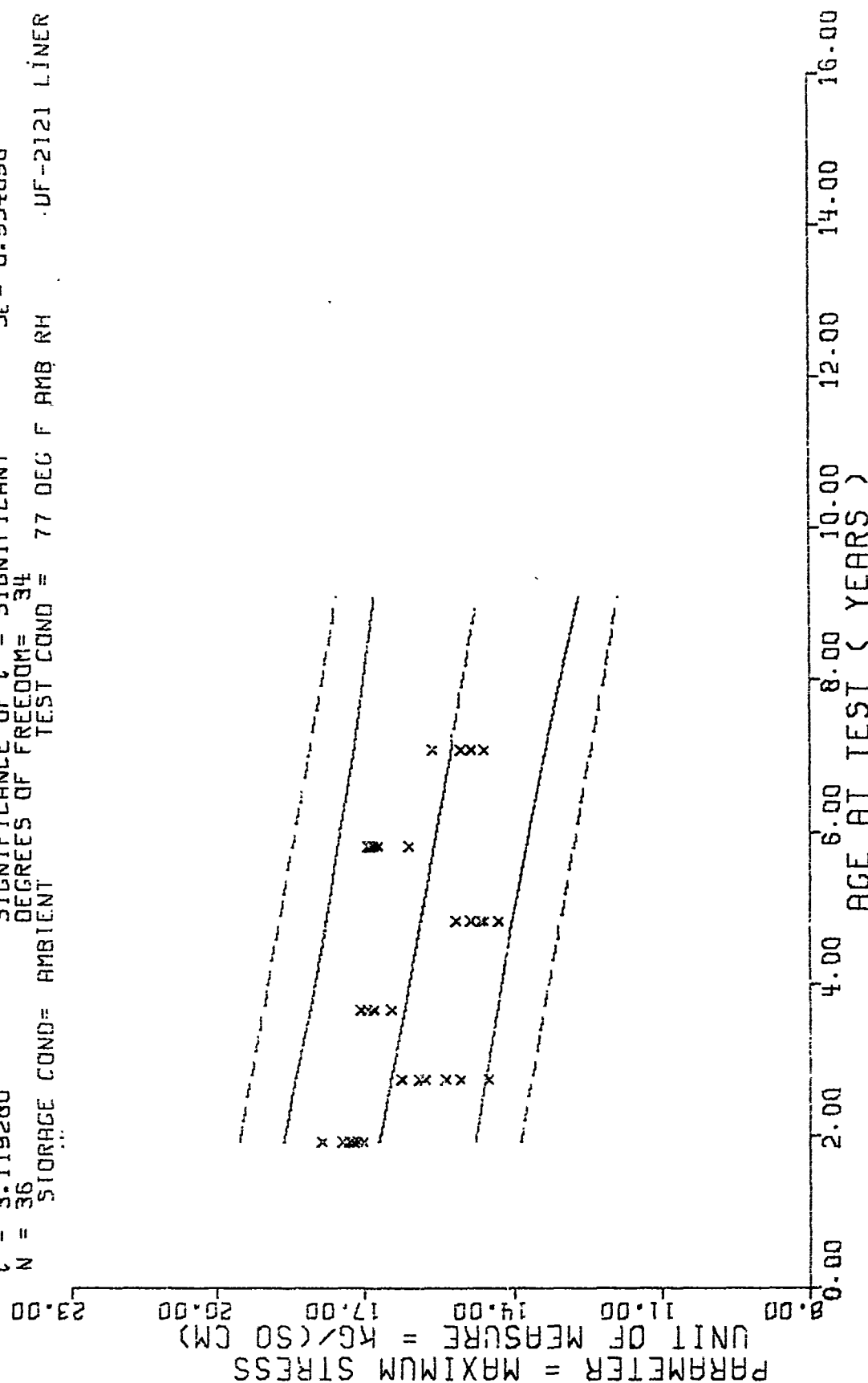
| DISC      |                    |         |                    | CUP     |                    |         |                    | PEEL    |         |         |         |
|-----------|--------------------|---------|--------------------|---------|--------------------|---------|--------------------|---------|---------|---------|---------|
| Control   |                    | Special |                    | Control |                    | Special |                    | Control |         | Special |         |
| Nr        | kg/cm <sup>2</sup> | Nr      | kg/cm <sup>2</sup> | Nr      | kg/cm <sup>2</sup> | Nr      | kg/cm <sup>2</sup> | Nr      | kg/L-cm | Nr      | kg/L-cm |
| 31        | 15.116             | 211     | 14.764             | 91      | 9.281              | 271     | 11.109             | 151     | 0.9465  | 331     | 1.1965  |
| 32        | 14.905             | 212     | 14.413             | 92      | 10.054             | 272     | 10.265             | 152     | 1.0179  | 332     | 1.1786  |
| 33        | 14.624             | 213     | 14.202             | 93      | 10.616             | 273     | 10.898             | 153     | 1.0715  | 333     | 1.1072  |
| 34        | 14.905             | 214     | 14.272             | 94      |                    | 274     | 10.687             | 154     | 1.1072  | 334     | 1.0536  |
| 35        | 15.678             | 215     | 13.870             | 95      | 9.894              | 275     | 9.491              | 155     | 1.0179  | 335     | 1.0358  |
| 36        | 15.116             | 216     | 14.272             | 96      | 10.054             | 276     |                    | 156     | 1.0715  | 336     | 1.0358  |
| $\bar{Y}$ | 15.057             |         | 14.284             |         | 9.998              |         | 10.490             |         | 1.0388  |         | 1.0846  |
| S         | 0.3539             |         | 0.3188             |         | 0.4750             |         | 0.6397             |         | 0.0569  |         | 0.0613  |

TABLE 8.  
ANALYSIS OF COVARIANCE RESULTS WHEN COMPARING  
CONTROL AND SPECIAL REGRESSION DATA

| Type of Data Compared | Parameter Compared | F-value | Degrees of Freedom | Significance    |
|-----------------------|--------------------|---------|--------------------|-----------------|
| Disc                  | Variance           | 1.83    | 34, 34             | significant     |
|                       | Slope              | 0.32    | 1, 68              | not significant |
|                       | Elevation          | 0.64    | 1, 69              | not significant |
| Cup                   | Variance           | 1.38    | 33, 31             | not significant |
|                       | Slope              | 0.20    | 1, 64              | not significant |
|                       | Elevation          | 0.06    | 1, 65              | not significant |
| Peel                  | Variance           | 1.49    | 34, 34             | not significant |
|                       | Slope              | 0.06    | 1, 68              | not significant |
|                       | Elevation          | 0.32    | 1, 69              | not significant |



F = 9.729911  
 R = -0.471699  
 U = 3.119280  
 N = 36  
 STORAGE COND= AMBIENT  
 Y = ( 17.288131 ) + ( -0.023334 ) \* X  
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF U = SIGNIFICANT  
 DEGREES OF FREEDOM= 34  
 TEST COND = 77 DEG F AMB RH .UF-2121 LINER



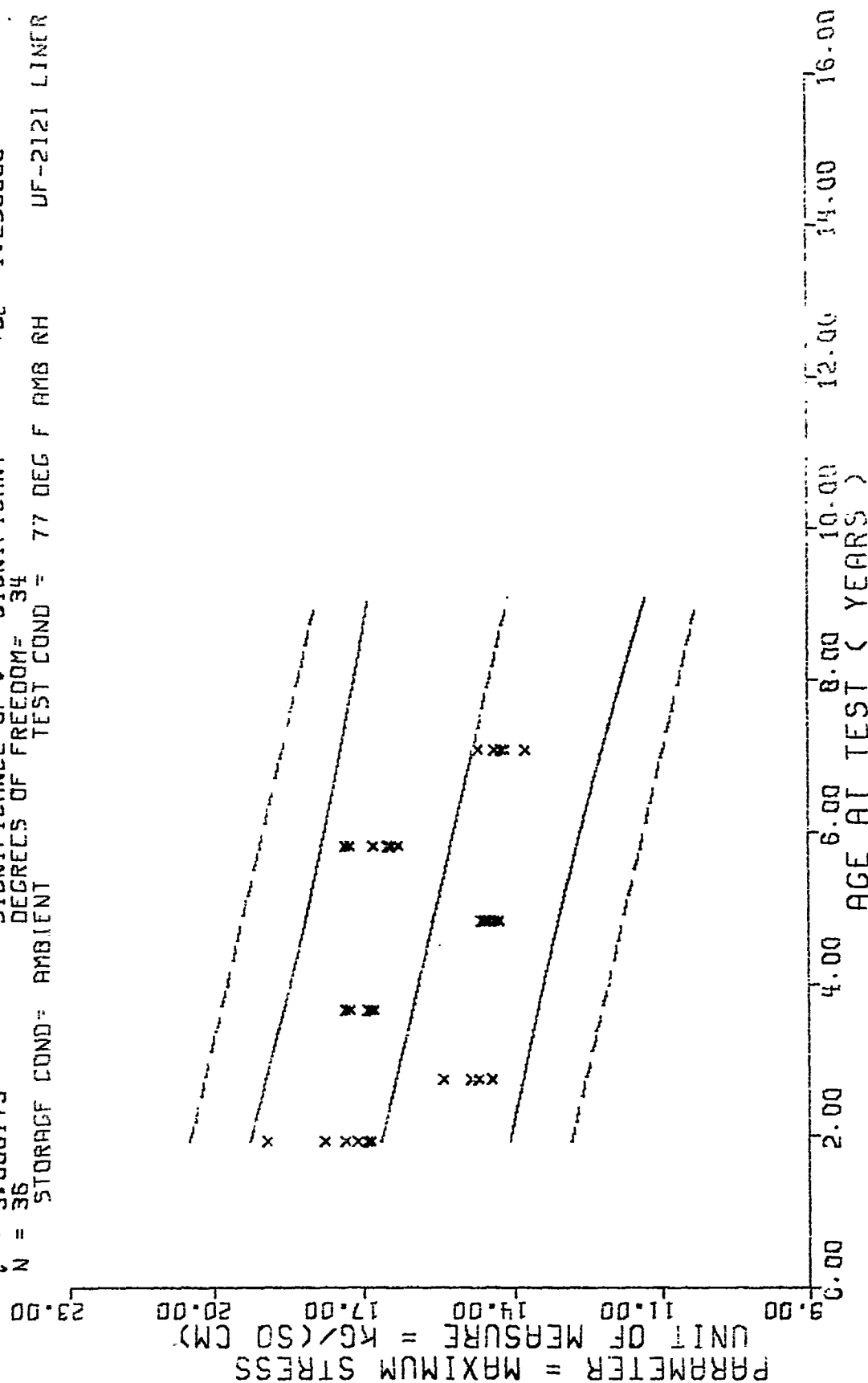
MAPQ. CONTROL DISC (STEEL/LINER/STEEL) TEST NR 6

Figure 1

```

F = 9.037075      ) + ( -0.030413      ) * X      QY = 1.430830
R = -0.458240     SIGNIFICANCE OF F = SIGNIFICANT      SQ = 0.010117
U = -3.006173     SIGNIFICANCE OF R = SIGNIFICANT      SE = 1.290330
N = 36            SIGNIFICANCE OF U = SIGNIFICANT
                        DEGREES OF FREEDOM = 34
STORAGE COND= AMBIENT      TEST COND = 77 DEG F AMB RH      UF-2121 LINER

```



**Figure 2**

F = 19.427673  
 R = -0.620692  
 U = 4.407682  
 N = 33  
 STORAGE COND = AMBIENT  
 Y = ( 13.002456 ) + ( -0.043358 ) \* X  
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF U = SIGNIFICANT  
 DEGREES OF FREEDOM = 31  
 TEST COND = 77 DEG F AMB RH  
 UF-2121 LINER  
 QY = 1.459278  
 SD = 0.009837  
 SE = 1.162461

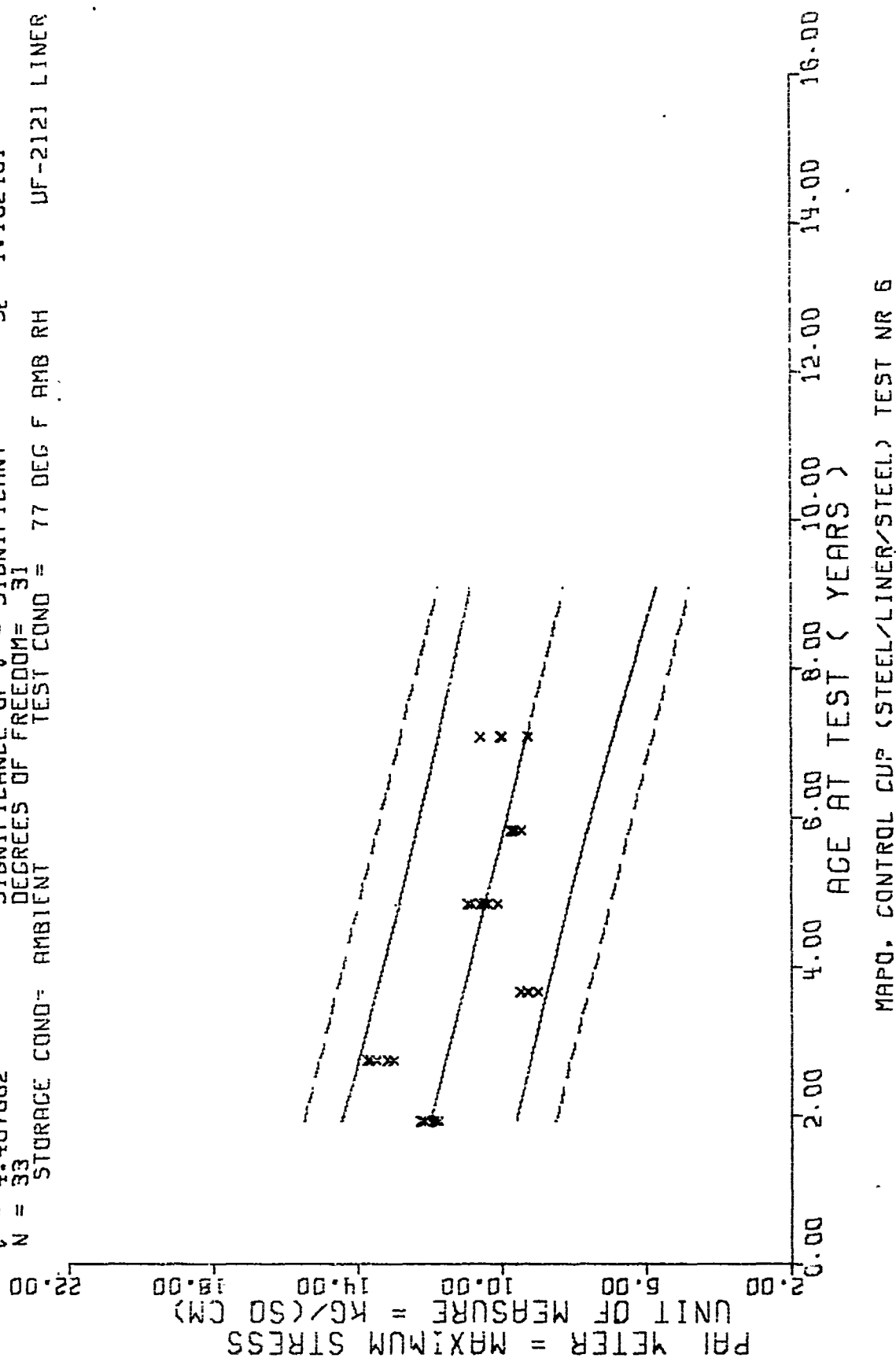


Figure 3

F = 10.241497  
 R = -0.499000  
 L = 3.307792  
 N = 35  
 STORAGE COND = AMBIENT  
 Y = ( 12.576515 ) + ( -0.036624 ) \* X  
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF L = SIGNIFICANT  
 DEGREES OF FREEDOM = 33  
 TEST COND = 77 DEG F AMB RH UF-2121 LINER

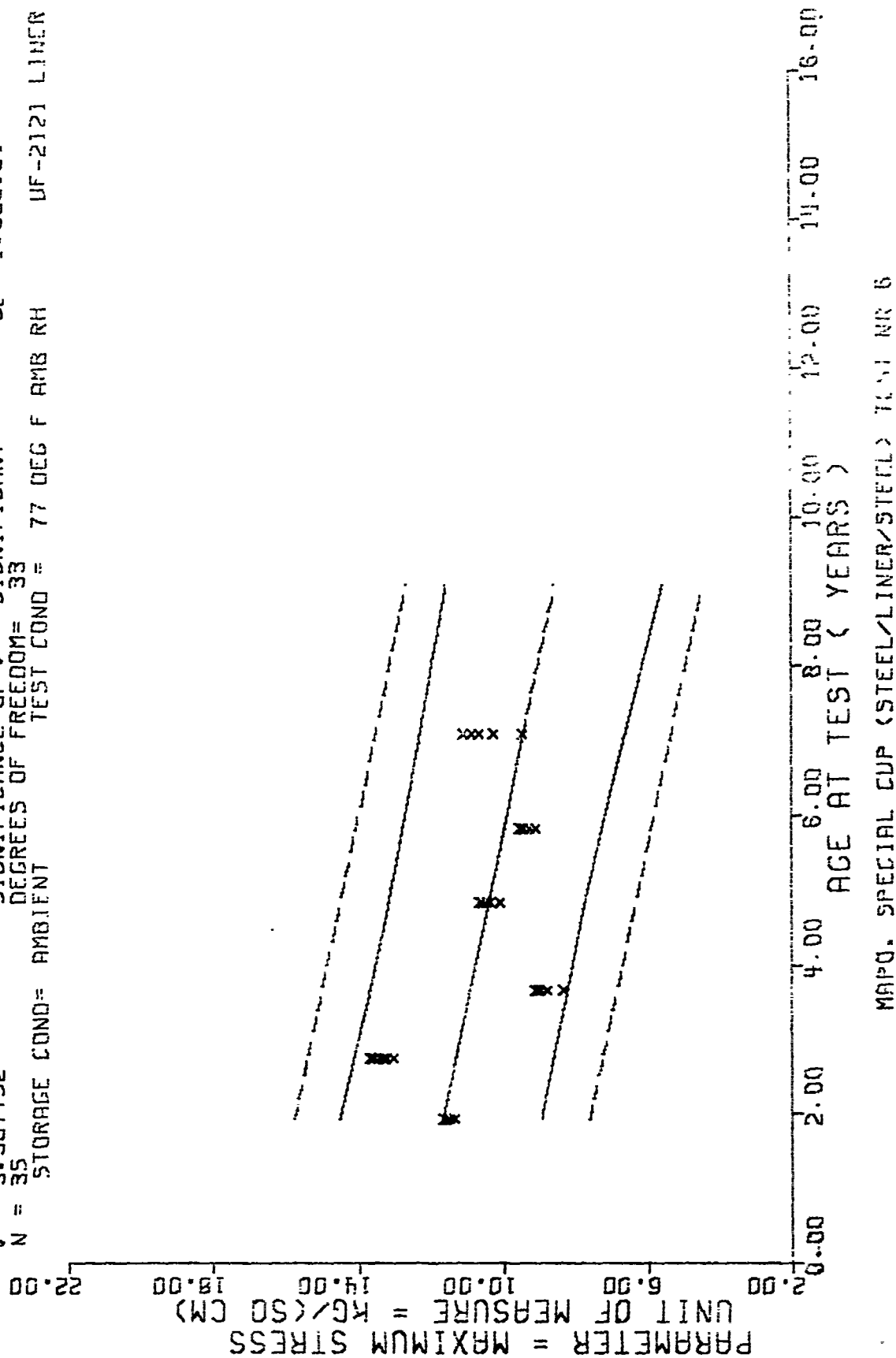
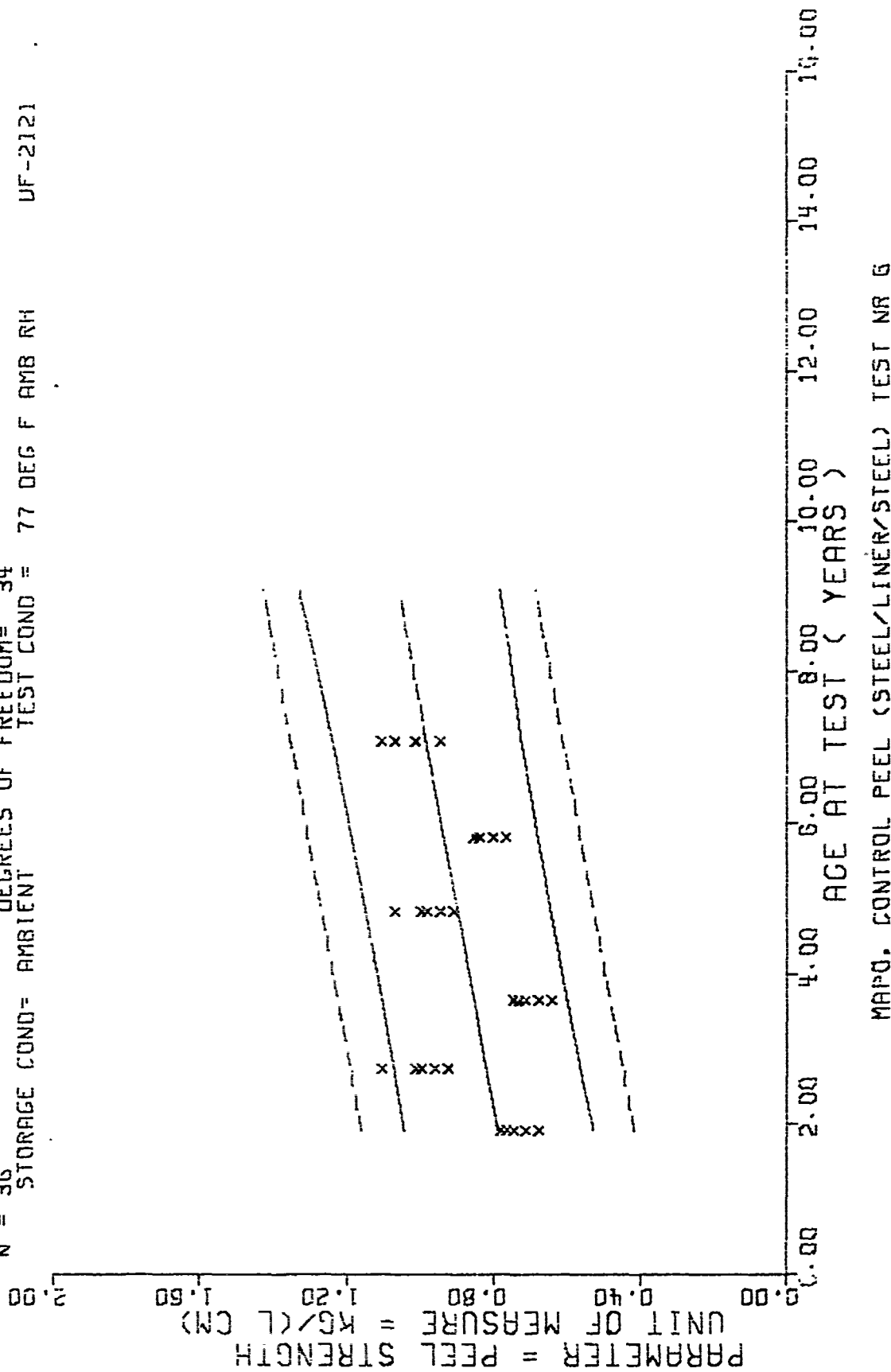


Figure 4

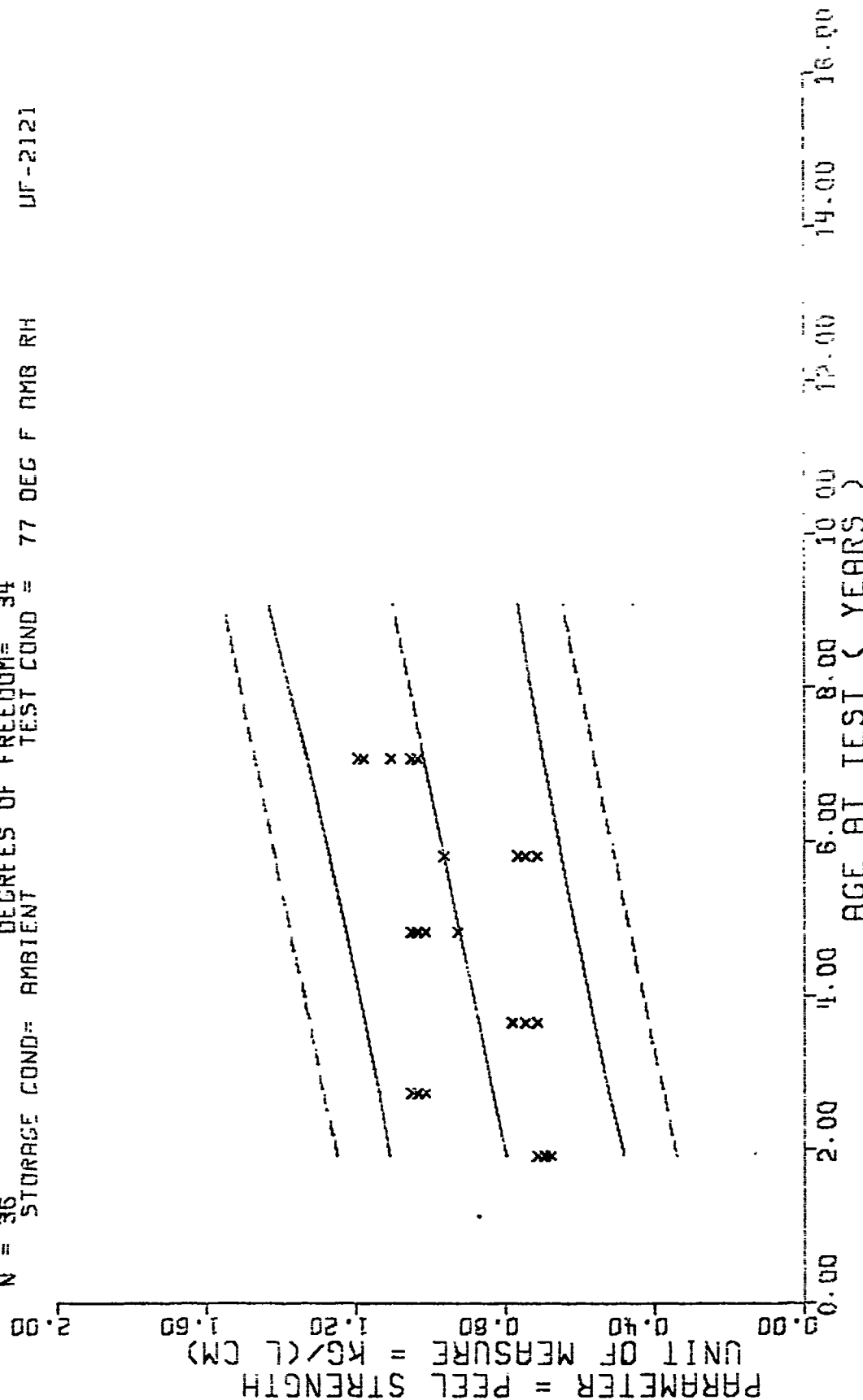
$F = 10.499542$   
 $R = 0.485744$   
 $t = 3.240299$   
 $N = 36$   
 STORAGE COND = AMBIENT  
 TEST COND = 77 DEG F AMB RH UF-2121

$Y = ( 0.715249 ) + ( 0.003150 ) * X$   
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM = 34

$CY = 0.139813$   
 $S_B = 0.000972$   
 $S_F = 0.123995$



F = 8.879981  
 R = 0.455070  
 t = 2.979929  
 N = 36  
 STORAGE COND= AMBIENT  
 Y = ( 0.713247 ) + ( 0.003540 ) \* X  
 SIGNIFICANCE OF F = SIGNIFICANT  
 SIGNIFICANCE OF R = SIGNIFICANT  
 SIGNIFICANCE OF t = SIGNIFICANT  
 DEGREES OF FREEDOM= 34  
 TEST COND = 77 DEG F AMB RH UF-2121



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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>Thiokol Chemical Corporation/Wasatch Division uses MAPO in the production of UF-2121 liner. Thiokol changed MAPO vendors and, therefore, qualification of the new source MAPO was required. Thiokol prepared specimens from the new source and also specimens from the original source which are to be used as the control material in the 10 year surveillance testing program. The specimens were transferred to Ogden ALC for testing and reporting of the data obtained. |   |  |



→ This report includes the test results for the first, second, third, fourth, fifth, and sixth time testing of the control and special specimens at OOALC.

Statistical analysis of the test data showed that the physical properties of the new source compared closely to the old source of UF-2121 liner specimens.

In all instances, the mean data for the control and special specimens are well above the minimum requirements found in TWR-7857 Rev A, Thiokol specimen data. Therefore, the capability of the liner from the new source material is expected to perform satisfactorily.